<u>Professor</u>: J.D. Wilson <u>Time available</u>: 120 mins <u>Value</u>: 35%

Please answer in the exam booklet. Some pertinent equations/data are given at the back.

## Multi-choice

 $(15 \ge 1\%) = 15\%$ 

- 1. If vectors  $\overrightarrow{u}$  and  $\overrightarrow{v}$  have representation  $\overrightarrow{u} = (\alpha, 0, 1)$  and  $\overrightarrow{v} = (0, 1, \beta)$  when projected onto orthogonal unit vectors  $(\hat{i}, \hat{j}, \hat{k})$ , then their inner product  $\overrightarrow{u} \bullet \overrightarrow{v} =$ \_\_\_\_\_
  - (a) 0
  - (b) 1
  - (c)  $\alpha$
  - (d)  $\beta \quad \checkmark \checkmark$
  - (e)  $\alpha\beta$
- 2.  $\alpha_i$  and  $\tau_{ij}$  are respectively rank 1 and rank 2 (Cartesian) tensors in a 2-D space. Under the summation convention the quantity  $\alpha_i \partial \tau_{ij} / \partial x_j$  expands to
  - (a)  $\alpha_1 \partial \tau_{12} / \partial x_1$
  - (b)  $\alpha_2 \ \partial \tau_{21} / \partial x_2$
  - (c)  $\alpha_1 \partial \tau_{11} / \partial x_1 + \alpha_1 \partial \tau_{12} / \partial x_2 + \alpha_2 \partial \tau_{21} / \partial x_1 + \alpha_2 \partial \tau_{22} / \partial x_2 \quad \checkmark \checkmark$
  - (d)  $(\alpha_1 \alpha_2) (\partial \tau_{11} / \partial x_1 + \partial \tau_{22} / \partial x_2)$
  - (e)  $(\alpha_2 \alpha_1) (\partial \tau_{11} / \partial x_1 + \partial \tau_{22} / \partial x_2)$
- 3. The Von Neumann stability analysis of a finite-difference discretization scheme covers \_\_\_\_\_ but does not account for \_\_\_\_\_
  - (a) any d.e. (differential eq'n) expressed in Cartesian coordinates; time-dependence
  - (b) any linear d.e.; boundary conditions  $\checkmark \checkmark$
  - (c) first- or second-order d.e.'s only; non-linearity
  - (d) any linear d.e.; influence of unresolved scale of motion
  - (e) heat/diffusion type equations; inhomogeneities (Q- type terms)

4. The von Neumann analysis of  $\frac{\partial c}{\partial t} = -U \frac{\partial c}{\partial x}$  results in a criterion on the \_\_\_\_\_ number

- (a) Diffusion
- (b) Reynolds
- (c) Richardson
- (d) Courant  $\checkmark \checkmark$
- (e) Euler
- 5. Which name(s) is/are associated with numerical schemes for solving the heat equation
  - (a) Crank and Nicolson
  - (b) Richardson
  - (c) Dufort
  - (d) Frankel
  - (e) all of the above  $\checkmark \checkmark$
- 6. The shortest wave that can be represented on a grid with spacing  $\Delta x$  has wavelength
  - (a)  $\pi/\Delta x$
  - (b)  $2\pi/\Delta x$
  - (c)  $\Delta x/2$
  - (d)  $\Delta x$
  - (e)  $2\Delta x \quad \checkmark \checkmark$

7. If  $S_x(f)$  is the power spectrum of a random variable x(t), then  $\int_0^\infty S_x(f) df =$ 

- (a) 0
- (b)  $\infty$
- (c)  $\Delta x$ , the grid interval
- (d)  $\Delta t$ , the time step
- (e)  $\sigma_x^2$ , the variance of  $x(t) \quad \checkmark \checkmark$
- 8. If the Fourier transform of T(x,t) satisfies  $\partial/\partial t \ \widetilde{T}(k,t) = -K \ k^2 \ \widetilde{T}(k,t)$  where k is wavenumber and K is a constant, then T must be governed by a/n \_\_\_\_\_
  - (a) advection equation
  - (b) diffusion equation  $\checkmark \checkmark (1)$
  - (c) advection-diffusion equation
  - (d) time-independent equation  $\checkmark \checkmark (1/2)$
  - (e) inhomogeneity

- 9. In relation to the above question, the Fourier mode T(k,t) must \_\_\_\_\_
  - (a) grow logarithmically in proportion to  $(Kk^2t)$
  - (b) grow exponentially in proportion to  $Kk^2t$
  - (c) decay in proportion to  $\sqrt{Kk^2t}$
  - (d) decay exponentially in proportion to  $Kk^2t \quad \checkmark \checkmark$
  - (e) vanish
- 10. Suppose  $L[\phi(x)] = 0$  (where L[] is a differential operator) is to be solved on  $a \leq x \leq b$  using the Bubnov-Galerkin method with basis functions  $\theta_j(x)$ . The expansion coefficients  $a_j$  are optimized by requiring that \_\_\_\_\_
  - (a)  $a_i a_j = \delta_{ij}$
  - (b) the residual  $e(x) = L\left[\sum_{j=1}^{N} a_j \theta_j(x)\right]$  must vanish
  - (c) the residual e(x) must be minimal
  - (d) the residual e(x) must be uncorrelated with each  $\theta_j(x)$  over  $a \le x \le b$   $\checkmark \checkmark$
  - (e) all of the above
- 11.  $Q_c$  is the mean vertical flux density of an admixture 'c' across the atmospheric surface layer (friction velocity  $u_*$ , Obukhov length L). According to the Monin-Obukhov similarity theory, statistics of c (like its standard deviation,  $\sigma_c$ ) scale with \_\_\_\_\_
  - (a)  $u_*$
  - (b) L
  - (c)  $u_*L$
  - (d)  $Q_c/L$
  - (e)  $Q_c/u_* \checkmark \checkmark$
- 12. Consider the kinetic energy k of the unresolved motion in a horizontally-uniform layer of the atmosphere that is in local equilibrium (conservation equation given at back): if the layer is stably stratified then buoyant production \_\_\_\_\_
  - (a) tends to increase k
  - (b) has the same sign as shear production
  - (c) vanishes
  - (d) balances shear production
  - (e) when summed with shear production, balances viscous dissipation  $\epsilon \quad \checkmark \checkmark$

- 13. The hemispheric irradiance across a unit of area whose normal is oriented vertically (ie. parallel to unit vector  $\hat{k}$ ) is given by  $F_z = \int_{\theta=0}^{2\pi} \int_{\phi=0}^{\pi/2} I(\hat{s}) (\hat{k} \bullet \hat{s}) \sin \phi \, d\theta \, d\phi$  where  $\hat{k} \bullet \hat{s} = \cos \phi$ . If the radiation intensity I is isotropic then  $F_z =$  \_\_\_\_\_
  - (a) 0
  - (b)  $1/2 \sin(2\phi)$
  - (c)  $\pi I \qquad \checkmark \checkmark$
  - (d)  $2\pi I$
  - (e)  $4\pi I$
- 14. Let X(t) denote the displacement (along direction x) of a particle from its point of release at time t = 0. Assuming the motion is "diffusive" (with diffusivity K) then (over an ensemble of trials) the statistic  $\sigma_x^2(t) \equiv \overline{(X(t) \overline{X}(t))^2} =$ 
  - (a) 0
  - (b)  $\sqrt{2Kt}$
  - (c)  $2Kt \quad \checkmark \checkmark$
  - (d)  $(2K t)^2$
  - (e)  $\infty$

15. The colour of the (unpolluted, cloudless) sky is explained by the \_\_\_\_\_

- (a) wavelength  $(\lambda)$  selectivity of the Rayleigh scattering function
- (b) anisotropy of the Rayleigh scattering function
- (c) wavelength selectivity of the Mie scattering function
- (d) anisotropy of the Mie scattering function
- (e) wavelength-dependence of the (Rayleigh) single scattering albedo  $(\omega_o\propto\lambda^{-4})$   $\checkmark\checkmark$

## Short answer:

 $4 \ge 5\% = 20\%$ 

Answer any **four** questions from this section, writing a (**maximum**) of one page per question. Additional pages used for calculations/working/preparation will not be marked. (**Turn to the back for answers**)

1. Explain the meaning and implications of the term "neutrally-stratified" as applied to the atmospheric boundary-layer, making reference both to the mean vertical flux density of sensible heat  $(Q_H)$  and the vertical temperature (or potential temperature) gradient. You may assume a dry atmosphere. Explore the implications of neutrality with regard to the kinetic energy budget (to this end you may assume steady state and local equilibrium apply; the equations given as data should help).

2. In the symbolic computing language of your choice, write down a code to evaluate the formula

$$T(y) = \sum_{i=1}^{20} \sum_{j=i}^{20} (-1)^{i+j} \sin(\pi y)$$

for a set of real values of y stored in the array x(k), viz. y = x(k), k = (1, 2, ...10). Your code need not be executable and need not be in perfect syntax, but all major tasks except I/O must be addressed, including declaration (typing) of the variables.

3. Suppose  $\phi = \phi(x, y)$  is defined in the quadrant  $x, z \ge 0$  where it is governed by the differential equation (d.e.)

$$U\frac{\partial\phi}{\partial x} = \frac{\partial^2\phi}{\partial z^2}$$

(U > 0 is a real constant) and that this equation is to be solved on a uniform grid whose nodes (i, j) lie at  $x(i) = (i - 1)\Delta$ ,  $z(j) = (j - 1)\Delta$ . We may let  $\phi_{ij}^n$  denote the  $n^{th}$  iteration towards the solution away from a first guess field  $\phi_{ij}^0$ .

Discuss the need for (as yet unspecified) boundary conditions in order to fully pose (specify) this problem. Explain whether, if we wished to compute the solution for all  $0 \le x \le L$ , it would be adequate to invoke a single boundary condition on the x-axis at x = L, i.e. specify  $\phi(L, z)$ ? Classify the terms in the d.e., and address whether (and why) each of the spatial axes is 'one-way' or 'two-way'.

If we impose  $(\partial \phi / \partial z) = 1$  along z = 0 then after the 4<sup>th</sup> iteration the influence of this boundary condition will have propogated along the z(j) axis as far as which gridpoint (j), and why?

4. The lowest order finite difference approximation for  $\partial^4 \phi / \partial x^4$  is

$$\frac{\partial^4 \phi}{\partial x^4} = \frac{\phi(x+2\Delta) - 8\phi(x+\Delta) + 20\phi(x) - 8\phi(x-\Delta) + \phi(x-2\Delta)}{\Delta^4} + O(\Delta^2)$$

Without worrying about whether it will be numerically stable, formulate an explicit

algorithm to solve the differential equation

$$\frac{\partial \phi}{\partial t} = a \; \frac{\partial^4 \phi}{\partial x^4}$$

(where t is time and x is a spatial coordinate). Your algorithm need only be valid at 'interior' gridpoints, i.e. those distant no less than  $2\Delta$  from the edges of the domain.

Suppose instead you formulated an *implicit* discretization such that (in matrix representation) your scheme for advancing the solution over one timestep was  $\phi^{n+1} = \mathbf{A} \phi^n$ . Explain how many non-zero diagonals would appear in the coefficient matrix  $\mathbf{A}$ .

5. In a typical weather model whose lowest gridpoint lies in the atmospheric surface layer at  $z = z_a$ , the surface-atmosphere flux of heat  $(Q_{H0})$  is computed as

$$Q_{H0} = \rho c_p C_M C_H u_a (T_0 - T_a)$$

Explain the logic of this parameterization, defining all the terms in the above equation. Explain, too, how coefficients  $C_M, C_H$  are "calibrated."

6. Using the control volume method, discretize the differential equation

$$0 = \frac{d}{dz} \left( K(z) \frac{dC}{dz} \right) + q_1 \,\delta(z-h)$$

on the domain  $0 \le z \le L$  (where L >> h), assuming boundary conditions

$$C(L) = 0$$

$$\left(-K \frac{dC}{dz}\right)_{(z=0)} = q_2$$

 $(q_1, q_2 \text{ are constants that are not necessarily dimensionless})$ . State the neighbour coefficients for an arbitrary internal control volume (ie. not at or adjacent to a boundary), and give a diagram of your grid (including uppermost and lowermost control volumes) that clarifies your procedure. Give also a physical interpretation of the governing equation, ie. explain speculatively what physical problem it models.

Data:

•

$$\frac{k_v z}{u_*} \frac{\partial \overline{u}}{\partial z} = \phi_m \left(\frac{z}{L}\right) \tag{7}$$

Dimensionless mean wind shear in the horizontally-uniform atmospheric surface layer, given by the universal Monin-Obukhov function on the r.h.s. (which in neutral stratification, i.e. at |z/L| = 0, has the limit  $\phi_m(0) = 1$ ). Similar expressions apply for gradients in mean temperature, humidity, etc.

$$L = \frac{-u_*^3}{k_v \frac{g}{T_0} \overline{w'T'}}$$

Definition of the Obukhov length, where:  $u_*$  is the friction velocity,  $k_v$  is the von Karman constant,  $T_0$  [K] is the mean temperature of the atmospheric surface layer, and  $\overline{w'T'}$  [ $\equiv Q_H/(\rho c_p)$ ] is the mean vertical (kinematic) flux density of sensible heat.

• The kinetic energy of the unresolved motion  $u'_i = (u', v', w')$  is by definition  $k = (\overline{u'^2} + \overline{v'^2} + \overline{w'^2})/2$ . In a horizontally-homogeneous layer the conservation equation for k, in a coordinate system aligned with the mean wind, is:

$$\frac{\partial k}{\partial t} = -\overline{u'w'} \frac{\partial U}{\partial z} + \frac{g}{T_0} \overline{w'T'} - \epsilon + \frac{\partial}{\partial z} \overline{w'} \left(\frac{p'}{\rho} + \frac{1}{2} \left(u'^2 + v'^2 + w'^2\right)\right)$$

Here  $\epsilon$  is the 'rate of dissipation of unresolved kinetic energy' and terms have their usual meaning.

• The heat flux budget equation in a horizontally-homogeneous layer is

$$\frac{\partial \overline{w'T'}}{\partial t} = -\overline{w'^2} \frac{\partial \overline{T}}{\partial z} - \frac{\partial}{\partial z} \overline{w'w'T'} - \frac{1}{\rho_0} \overline{T'\frac{\partial p'}{\partial z}} + \frac{g}{T_0} \overline{T'^2}$$
(10)

where  $\rho_0, T_0$  are the mean density and (Kelvin) temperature of the layer. It is often assumed that at steady state this reduces to a balance between the first term on the r.h.s. (gradient production: a source term) and the  $T' \frac{\partial p'}{\partial z}$  covariance term, also a source term.

## Skeleton short answers

- 1. Regarding the "neutrally-stratified" atmospheric boundary-layer, any of these points would gain you a mark:
  - $Q_H = 0$ , or alternatively  $\overline{w'T'} = 0$
  - $\partial \overline{T}/\partial z \gamma_d = 0$ , where  $\overline{T}$  is the **mean** temperature; alternatively  $\partial \overline{\theta}/\partial z = 0$ , where  $\overline{\theta}$  is the **mean** potential temperature (since in principle the temperature fluctuations vanish, no penalty for failing to specify 'mean')
  - no buoyant production in TKE equation, so (at local equilibrium and steady state)  $\epsilon = -\overline{u'w'} \partial U/\partial z$  (a half mark if you got part way to this result)
  - in the surface layer the MO scale  $T_* = -Q_H/u_*$  for temperature fluctuations vanishes... no temperature fluctuations
  - in the surface layer the MO length scale  $|L| = \infty \ (z/L = 0)$
  - parcels displaced in the vertical experience no consequent buoyancy force
  - neutral ABL can be said to be "well-mixed"
- 2. Evaluate  $T(y) = \sum_{i=1}^{20} \sum_{j=i}^{20} (-1)^{i+j} \sin(\pi y)$  for a bunch of values of y. What was tested here was your familiarity with nested loops, and the type of variable generally called an "accumulator" (here named "sum"). Marked by subtracting  $\frac{1}{2}$  for each mistake. Common mistakes were: wrong lower limit for the j loop; failure to actually so the summation (as marked 'wrong' below) with result that computation yields only the contribution from i = j = 20.

```
integer i,j
real pi,sum,y,x(10)
pi=3.14159
read x(k) for k=1,..10 (optional)
do k=1,10
  y=x(k)
  sum=0.0
  do i=1,20
     do j=i,20
     sum=sum+((-1)**(i+j))*sin(pi*y)
     sum=((-1)**(i+j))*sin(pi*y) wrong!
  end do
```

С

3. The  $U\frac{\partial\phi}{\partial x} = \frac{\partial^2\phi}{\partial z^2}$  problem. Marked by assigning +1 per point below (to max of 5)

- to fully pose the problem (ie. render it definite and so solvable) we need 1 b/c on the x-axis and 2 on the z-axis
- on the z-axis, the problem is 'elliptic' ('jury' problem), this is a '2-way' axis
- however the x-axis is a '1-way' axis, and the solution φ<sub>i,j</sub> at gridpoint (i, j) can be affected only by the upstream field φ<sub>i-1,k</sub> (if we take the simplest discretization of the Laplacian term, the upstream influence is restricted to height range j − 1 ≤ k ≤ j + 1)
- An advection term  $U\partial\phi/\partial x$  is best discretized using an 'upwind' difference (ie. if I want  $\partial\phi/\partial x$  where I am standing with my back to the wind, I take the value of  $\phi$  where I am minus the value behind my back, and divide by the distance)... this captures the '1-way' character of the transport process. From the physical perspective a boundary condition at x = L would not work (it could not influence the solution at x < L). However since I did not clearly teach and give you notes on this point (inferiority of a downwind difference for advection) and because mathematically, by choosing a downwind difference for the advection term, one could obtain a solution even if one imposed the b/c at x = L, I accepted either argument.
- since U = const both terms in the d.e. are transport terms, i.e. can be written as the spatial derivative of a flux
- The simplest discretization for the Laplacian term (φ<sub>i,j+1</sub> + φ<sub>i,j-1</sub> 2φ<sub>i,j</sub>)/Δ<sup>2</sup> is going to zip the influence of the lower boundary condition upwards along the z (ie. j) axis by one gridpoint per iteration. So after 4 iteration the boundary influence is felt up to the 4<sup>th</sup> internal gridpoint; however since there can be ambiguities about the counting here, I did not insist on 4

- Since this is (or can be formulated as) a marching problem on the x-axis, iteration is not actually necessary... but then the influence of the lower boundary will propagate up the j-axis by one gridpoint for each downstream step taken
- 4. Letting  $\phi_i^n$  represent the solution at time  $n\Delta t$  and location  $i\Delta$ , an explicit algorithm for  $\frac{\partial \phi}{\partial t} = a \frac{\partial^4 \phi}{\partial x^4}$  would be

$$\frac{\phi_i^{n+1} - \phi_i^n}{\Delta t} = \frac{a}{\Delta^4} \left( \phi_{i+2}^n - 8\phi_{i+1}^n + 20\phi_i^n - 8\phi_{i-1}^n + \phi_{i-2}^n \right)$$

so in terms of neighbour coefficients we have (3 marks)

 $\phi_i^{n}$ 

$${}^{+1} = + \gamma \phi_{i-2}^{n} - 8\gamma \phi_{i-1}^{n} + (1 + 20\gamma) \phi_{i}^{n} - 8\gamma \phi_{i+1}^{n} + \gamma \phi_{i+2}^{n}$$

where  $\gamma = a\Delta t/\Delta^4$ . Because this algorithm requires values at gridpoints i - 2, i - 1, i, i + 1, i + 2 there would be 5 non-zero diagonals in the coefficient matrix of an implicit formulation (2 marks).

5. Interpreting/explaining the boundary flux parameterization  $Q_{H0} = \rho c_p C_M C_H u_a (T_0 - T_a)$ .

- formulation assumes the sensible heat flux density  $Q_{H0}$  is 'driven' by the (model's) surface-to-air temperature difference  $(T_0 - T_a)$
- but we need to multiply by a velocity to get units of kinematic heat flux, and  $u_a$ (model's mean horizontal windspeed at  $z = z_a$ ) is available from the model (other choices of a windspeed 'known to the model' would be possible, but would result in different coefficients)
- the factor  $\rho c_p$  converts our kinematic heat flux density into the units [W m<sup>-2</sup>]
- to get the (dimensionless) coefficients, we turn to Monin-Obukhov similarity theory (MOST), which is appropriate for a horizontally uniform surface layer

(since our model doesn't resolve the surface layer on a scale finer than its grid, the assumption of horizontal uniformity that is implicit in MOST is consistent with the modelling approach). We start by noting that according to MOST

$$\frac{k_v z}{u_*} \frac{\partial \overline{u}}{\partial z} = \phi_m \left(\frac{z}{L}\right)$$
$$\frac{k_v z}{T_*} \frac{\partial \overline{T}}{\partial z} = \phi_h \left(\frac{z}{L}\right)$$

where  $T_* = -Q_{H0}/(\rho c_p u_*)$  and  $\phi_h$  is the universal MO function for heat (the first of these equations was given as data). Re-arrange the second of these formulae

$$\frac{\partial \overline{T}}{\partial z} = \frac{-Q_{H0}/(\rho c_p u_*)}{k_v z} \phi_h(z/L)$$

and upon integrating from the surface to  $z = z_a$ 

$$T_a - T_0 = \frac{-Q_{H0}/(\rho c_p u_*)}{k_v} \int_0^{z_a} \phi_h(\frac{z}{L}) \frac{dz}{z}$$

we have a formula linking  $Q_{H0}$  to  $(T_0 - T_a)$  that can be used to determine  $C_M C_H$ (the coefficient  $C_M$  enters when we re-express  $u_*$  as a multiple of  $u_a$ )

6. Control volume discretization of  $0 = \frac{d}{dz} \left( K(z) \frac{dC}{dz} \right) + q_1 \delta(z-h).$ 

- We have a steady-state, 1-d diffusion problem. There is a source (strength  $q_1$ ) of the property C inside the domain at z = h, and another (strength  $q_2$ ) at the lower boundary z = 0 (since we have a prescribed flux at that boundary). The top boundary z = L is either very remote from the sources, or (better interpretation) is a perfect sink
- define a uniform grid along the z axis with gridlength  $\Delta$
- index the gridpoints (j)
- sketch the grid giving definitions
- integrate the d.e. over the interval  $z_s \leq x \leq z_n$  where  $z_s, z_n$  are the upper and lower boundaries to the control volume (or control layer) associated with gridpoint
  - j. In view of the  $\delta$ -function multiplying the source term, the result is

$$0 = \left[ K(z) \ \frac{dC}{dz} \right]_{z_s}^{z_n} + \ q_1 \delta_{jj_h}$$

where  $\delta_{jjh}$  vanishes unless layer j encloses the source at z = h (in which case it is unity)

• Introducing central differences we have

$$0 = K(z_n) \frac{C_{j+1} - C_j}{\Delta} - K(z_s) \frac{C_j - C_{j-1}}{\Delta} + q_1 \delta_{jj_h}$$

or rearranging

$$C_j \left[\frac{K_n}{\Delta} + \frac{K_s}{\Delta}\right] = C_{j-1} \frac{K_s}{\Delta} + C_{j+1} \frac{K_n}{\Delta} + q_1 \delta_{jj_h}$$