

Tables (1, 2) give the mean wind ( $U$ ) and temperature ( $T$ ) profiles observed on a tower at Ellerslie, Alberta, in the middle of a flat field of sparse stubble during a fifteen minute period beginning 1345 MDT on June 1, 2001. Windspeed was measured with cup anemometers, which should be assumed to have overestimated the mean speed by 8%. Mean temperature *differences* relative to a reference level ( $z = 0.29$  m) were measured by shielded, ventilated thermocouples. One may assume the characteristic uncertainties in windspeed and temperature difference are  $\delta_u = 0.05$  m s<sup>-1</sup> and  $\delta_T = 0.1$  °C.

A wind vane determined that the mean wind direction (expressed in the ordinary compass convention)  $\beta_v = 138^\circ$ . A sonic anemometer at  $z = 2.2$  m determined the data given in Table (3).

**Aim:** The mean profiles define the state of the undisturbed ASL. From the given data, estimate for this period: the friction velocity  $u_*$ , the temperature scale  $T_*$ , the Monin-Obukhov length  $L$ , the sensible heat flux density<sup>1</sup>  $Q_H$ . Plot the given mean profiles, along with the theoretical profiles implied by your derived  $u_*, T_*$ .

From the sonic data compute alternative estimates  $u_*^s, T_*^s, L^s$  and mean wind direction  $\beta_s = \arctan(V/U)$  (correct for the orientation of the sonic frame, ie. add  $90^\circ$ ). Comment on the measured values of  $\sigma_u/u_*, \sigma_v/u_*, \sigma_w/u_*$  in the context of MO similarity theory.

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<sup>1</sup>The mean temperature  $T_0$  during this period was about 21° C, and for the purpose of calculating the density  $\rho_0$  you may assume the atmospheric pressure  $p = 93$  kPa.

## Profile Fitting Method

Correct the cup anemometers for overspeeding. Create the set of measured differences  $\Delta U_z^m = U_z - U_{ref}$ ,  $\Delta T_z^m = T_z - T_{ref}$  (etc.) where  $U_{ref}$  is the windspeed at a reference height, such as  $z = 0.65$  m. To each of these differences there correspond (for any guess of the scales  $u_*, T_*$ ) theoretical differences  $\Delta U_z^t = (U_z - U_{ref})^t$  (etc.) that may be calculated from the Monin-Obukhov similarity profiles. Your scales should be optimal in the sense that they minimise the dimensionless residual:

$$R = \frac{\sum_1^{N_U} (\Delta U^m - \Delta U^t)^2}{\delta u^2} + \frac{\sum_1^{N_T} (\Delta T^m - \Delta T^t)^2}{\delta T^2} \quad (1)$$

Here  $\delta u, \delta T$  are estimated instrument inaccuracy. In the present case the number of velocity differences is  $N_U = 4$  and  $N_T = 2$ .

## Data

Table 1: Profile of (uncorrected) mean cup windspeed, Ellerslie (AB), 1345-1400 hrs, 1 June, 2001.

$z$ [m]	$U(z)$ [m s <sup>-1</sup> ]
6.05	11.53
3.6	10.52
2.12	9.68
1.12	8.28
0.65	7.45

Table 2: Profile of mean temperature difference from reference temperature, Ellerslie (AB), 1345-1400 hrs, 1 June, 2001.

$z$ [m]	$T(z) - T(0.29\text{m})$ [°C]
5.75	-3.09
1.35	-1.52
0.29	0.00

Table 3: Statistics from the sonic anemometer at  $z = 2.2$  m over same interval. The sonic was ‘facing’ east, thus when  $v = 0$  wind direction is 90°. In principle, the statistics should be rotated into a frame for which  $W = 0$ , but we shall neglect this step.

Property	Value [MKS units]
$\sqrt{u^2 + v^2}$	9.17
$U$	3.06
$V$	1.88
$W$	-0.23
$T$	16.8
$\overline{u'^2}$	2.191
$\overline{v'^2}$	3.357
$\overline{w'^2}$	0.506
$\overline{u'w'}$	-0.225
$\overline{v'w'}$	-0.416
$\overline{w'T'}$	0.287